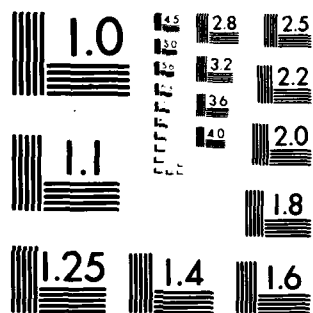


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# **SOME RAMIFICATIONS OF THE POWER-LAW SPECTRAL INDEX FOR PROPAGATION MODELING**

Charles L. Rino  
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1 October 1979

Topical Report for Period 1 January 1979— 30 September 1979

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This report discusses some ramifications for propagation modeling of these new theoretical results. The phase structure function and various functionals of it characterize the striation environment for predictive modeling. Two very different approximations to the phase structure function are currently being used.

One, an asymptotic approximation, is valid when the one-dimensional phase spectral density function falls off less rapidly than  $f^{-3}$ . The other, a quadratic approximation derived from the formal Taylor series expansion of the phase structure function, is valid when the one-dimensional phase spectral density function falls off more rapidly than  $f^{-3}$ .

The  $f^{-3}$  power law marks an important transition in the behavior of the complex signal moments. For the  $f^{-3}$  and more steeply sloped phase spectral density functions, the large-scale structure exerts a strong influence on the signal statistics. As a consequence, the outer scale cutoff, which is very difficult to determine, controls the signal parameters that are used to characterize the coherence time, coherence bandwidth, and so forth. This difficulty does not arise for the more shallowly sloped spectral density functions.

Attention is called to the fact that the Wideband satellite data have consistently shown phase spectral density functions that fall off less steeply than  $f^{-3}$ , whereas recent barium data from STRESS show more steeply sloped spectra. In light of the impact on propagation modeling, it is important that this discrepancy be resolved. Methods are suggested for testing the consistency of the data analysis procedures used to estimate the phase power-law index.

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## I INTRODUCTION

In this report the ramifications of some new theoretical results for modeling late-time, high-altitude nuclear propagation effects are discussed. The results are timely because it appears that there is a systematic difference between (1) the power-law index that characterizes the phase spectrum of radio waves that have propagated through a striated barium environment, and (2) the corresponding power-law index for most radio waves that have propagated through naturally occurring striations in both ionized and nonionized media.

It is generally assumed that the one-dimensional in-situ spectral density function (SDF) that characterizes both naturally occurring and barium striations has the form  $\kappa_x^{-2\pm?}$  (Ossakow, 1979)\*. For neutral turbulence in the inertial subrange, the Kolmogorov theory predicts  $\kappa_x^{-5/3}$ , whereas the nonlinear steepening of Rayleigh Taylor and  $E \times B$  coherent Fourier modes predicts  $\kappa_x^{-2}$ . The number of published in-situ data sets is sparse; however, recently analyzed STRESS data suggest  $\kappa_x^{-2.3}$  for barium striation.

If the local in-situ characterization of the irregularities applies throughout the propagation region, then the corresponding one-dimensional integrated-phase SDF has an index one larger than the one-dimensional in-situ index. Thus, the corresponding phase SDF should have the form  $f^{-3\pm?}$ . The Wideband satellite data have consistently shown comparatively shallow phase SDFs ( $f^{-p}$  with  $2.2 < p < 2.8$ ) at all latitudes under highly varied propagation conditions. Similar results are now being reported for interplanetary scintillation and line-of-sight microwave transmissions.

If one accepts the simple mapping from in-situ to phase structure, there is a discrepancy between the in-situ data and the scintillation data. Indeed, the scintillation data suggest an in-situ index smaller

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\*References are listed at the end of this report.

than the Kolmogorov value. There are good reasons why the simple mapping from in-situ to phase structure might not be invalid, but there is no question that it is the effective slope of the integrated phase SDF that determines the signal structure.

The new theoretical results we have alluded to show that there is a significant change in the signal statistics when the phase spectral slope approaches or exceeds 3. Indeed, the propagation modeling task is potentially much more difficult for steeply sloped spectra. In light of these new developments, it is important that the question of the appropriate effective spectral index for propagation modeling be resolved.

To introduce the problem, consider the common assumption that under conditions of sufficiently strong scatter, the complex signal  $v(t)$ , is Rayleigh distributed. This means formally that the quadrature components of  $v(t)$  are independent, identically distributed, gaussian random processes. Since the second-order statistics completely specify a gaussian random process, one need determine only the mutual coherence function

$$R_v(t, t') = \langle v(t)v^*(t') \rangle \quad (1)$$

to completely characterize the temporal structure of  $v(t)$  at a single frequency. In particular, all higher-order signal moments can be computed in terms of  $R_v(t, t')$ . For example,

$$\langle I(t)I(t') \rangle - \langle I(t) \rangle \langle I(t') \rangle = |R_v(t, t')|^2 \quad (2)$$

where

$$I(t) = |v(t)|^2 \quad (3)$$

is the signal intensity.

It follows from Eq. (2) that the  $S_4$  scintillation index  $[S_4^2 = (\langle I^2 \rangle - \langle I \rangle^2) / \langle I \rangle^2]$  is unity for a Rayleigh process. Thus, if  $S_4$  is not equal to unity, the Rayleigh limit does not apply. Insofar as systems

effects per se are concerned, departures from strict Rayleigh fading are not too serious (Johnson and Rino, 1979). The precise value of the spectral index, however, does impact predictions of time structure, frequency coherence, and so forth. A careful assessment of the signal structure is important, therefore, because it can verify the value that is assigned to the spectral index.

Indeed, Rino (1979b) showed that in a three-dimensional medium with an irregularity spectral density function (SDF) of the form  $C_s q^{-(2\nu+1)}$ ,  $S_4$  converges to unity in the strong-scatter limit if and only if  $\nu < 1.5$ . When  $\nu \geq 1.5$ ,  $S_4$  achieves a limiting value greater than unity, which can be determined from the formula

$$S_4^2 = \frac{4\sqrt{2\nu - 2}}{5 - 2\nu} \quad (4)$$

The value  $\nu = 1.5$  corresponds to a  $\kappa^{-2}$  one-dimensional in-situ SDF, which, as we have noted, is believed to be associated with steepened irregularity structures. If the  $\nu = 1.5$  structure model is assumed to have global applicability, then Eq. (4) predicts the strong-scatter limiting value  $S_4 = 1.4$ . Since this exceeds unity by 40%, it should be easily detected in any statistically valid data set. Strong focusing, which occurs before the limiting value is achieved, moreover, will cause even larger  $S_4$  values.

In addition to the purely phenomenological impact of the power-law slope, there are ramifications that should effect predictive codes. Indeed, the simple form that is being used for the phase structure function breaks down when  $\nu \geq 1.5$ .

What is happening can be described intuitively as follows: As the irregularity SDF steepens ( $\nu$  increases), the importance of the omnipresent large-scale structures steadily increases. If  $\nu < 1.5$ , these structures manifest themselves only in the first-order moments (e.g., as trend-like phase variations). If  $\nu \geq 1.5$ , the second-order moments (e.g., the mutual coherence function) develop trend-like components. Finally, if  $\nu \geq 2.5$ , even the fourth-order moments develop trend-like variations.

The Wideband satellite data clearly favor  $\nu$  values less than 1.5 as evidently do interplanetary scintillation data, and data from light and microwave propagation through turbulent atmospheres. To accommodate varying  $\nu$  values, however, a change in the usual approach to propagation modeling is required. Since the mutual coherence function plays a central role in the current approach to predictive modeling, we have developed the theory in detail in this report. The development shows clearly how inhomogeneities manifest themselves and what their impact on predictive modeling is.

## II THE MUTUAL COHERENCE FUNCTION

The differential equation that governs the development of the mutual coherence function is

$$\frac{dR_v(\vec{\rho}_1, \vec{\rho}_2)}{dz} = \frac{i}{2k} [\nabla_1^2 - \nabla_2^2] R_v(\vec{\rho}_1, \vec{\rho}_2) - \frac{1}{2} D(\rho_1, \rho_2) R_v(\vec{\rho}_1, \vec{\rho}_2) \quad (5)$$

In Eq. (5),  $\nabla_i^2 = \partial^2 / \partial \rho_{x_i}^2 + \partial^2 / \partial \rho_{y_i}^2$ ,  $k = 2\pi/\lambda$ , and  $D(\rho_1, \rho_2)$  is the incremental value of the phase structure function,

$$D(\vec{\rho}_1, \vec{\rho}_2) = \langle [\delta\phi(\vec{\rho}_1) - \delta\phi(\vec{\rho}_2)]^2 \rangle \quad (6)$$

As discussed by Rino (1978), all the moment equations derived from the parabolic wave equation by using the so-called Markov approximation contain two sets of terms. One set of terms, which involves the Laplacian  $\nabla_i^2$ , accounts for diffraction effects that act to generate small-scale structure in  $v(\vec{\rho})$ , particularly in its amplitude. The remaining terms account for the interaction of the wavefield with the randomly irregular medium.

Equation (5) is written in its isotropic form. The general form is developed in Rino (1978). The three-dimensional structure of the wavefield in an anisotropic medium can be derived by straightforward manipulations of the isotropic results (Rino and Fremouw, 1977; Rino, 1978, 1979a). Similarly, the temporal structure of  $v(\vec{\rho})$  is readily derived by using an appropriate velocity factor to convert spatial variations to temporal variations.

As a general rule, whenever the diffraction terms impact the solution, the particular moment will depend on the Fresnel factor  $\lambda z/4\pi$ . From Eq. (5), however, it is readily seen that if  $D(\vec{\rho}_1, \vec{\rho}_2)$  depends on the difference variable  $\vec{\Delta\rho} = \vec{\rho}_2 - \vec{\rho}_1$ , then  $R_v(\vec{\rho}_1, \vec{\rho}_2)$  depends only on  $\vec{\Delta\rho}$ , and

the diffraction terms cancel. It follows that the behavior of  $R_v(\vec{\rho}_1, \vec{\rho}_2)$  depends critically on the spatial homogeneity of the structure function.

In most radio-wave modeling work it is assumed without question that any departures of  $D(\vec{\rho}_1, \vec{\rho}_2)$  from strict homogeneity can be ignored. To illustrate that there is good reason to question this assumption, consider the signal mean  $\langle v(t) \rangle$ . The differential equation for  $\langle v(t) \rangle$  is

$$\frac{d\langle v(\vec{\rho}) \rangle}{dz} = \frac{-i}{2k} \nabla^2 \langle v(\vec{\rho}) \rangle - \frac{1}{2} r_e^2 \lambda^2 \langle \Delta N_e(\vec{\rho}) \rangle \langle v(\vec{\rho}) \rangle \quad (7)$$

If  $\langle \Delta N_e(\vec{\rho}) \rangle$  is strictly independent of  $\vec{\rho}$ , then  $\langle v(\vec{\rho}) \rangle$  is constant. In fact, one can easily obtain the solution to Eq. (7)--namely,

$$\langle v(\vec{\rho}) \rangle = \exp \left\{ -\frac{1}{2} \langle \delta \phi^2 \rangle \right\} \quad (8)$$

where

$$\langle \delta \phi^2 \rangle = r_e^2 \lambda^2 G \ell \int_0^z \langle \Delta N_e^2 \rangle d\ell \quad (9)$$

In Eq. (9)  $G$  is a purely geometrical factor and  $\ell$  is the first moment of the phase spectral density function.

Whether or not there is a spatial regime where  $\langle \Delta N_e(\vec{\rho}) \rangle$  can be considered to be constant can only be determined by careful data analysis. Detrending data establishes an arbitrary partitioning between large- and small-scale structures such that the detrended component exhibits all the properties of a homogeneous process. The absolute values of  $\langle \delta \phi^2 \rangle$  and  $\langle v(\vec{\rho}) \rangle$ , however, are determined by the detrend cutoff. In fact, analysis of the Wideband satellite data has shown that even with detrended data,  $\langle v(\vec{\rho}) \rangle$  is not well behaved. The estimates show a higher degree of dispersion than the corresponding  $S_4$  estimates. This suggests that the diffraction term in Eq. (7) cannot be ignored.

Going back to the mutual coherence function, if  $D(\vec{\rho}_1, \vec{\rho}_2)$  depends only on  $\Delta \vec{\rho}$ , then one can also easily obtain the solution to Eq. (5)--namely,

$$R_v(\vec{\Delta\phi}) = \exp \left\{ -\frac{1}{2} D_{\delta\phi}(\vec{\Delta\phi}) \right\} \quad (10)$$

where

$$D_{\delta\phi}(\vec{\Delta\phi}) = r_e^2 \lambda^2 \int_0^z D(\vec{\Delta\phi}) \, d\ell \quad . \quad (11)$$

We note that the initial condition  $R_v = 1$  at  $z = 0$  is implied by Eq. (10). This effectively normalizes the average signal intensity to unity.

From our experience with the first-order moments  $\langle \delta\phi^2 \rangle$  and  $\langle v \rangle$ , we take it as a guiding principle that whenever a computed signal moment of any order depends strongly on  $q_0$ , estimators of that quantity will be dependent on how they are measured. The effects are not simply due to uncertainties in the actual value of  $q_0$ , but rather to diffraction effects and/or inhomogeneities that can cause significant departures from the mathematical limiting form of the particular moment.

To pursue this further, in Section III we discuss the mathematical model that is being used for the phase structure function.

### III THE PHASE STRUCTURE FUNCTION

To simplify the analysis without loss of generality, let us assume that  $D(\vec{\rho}_1, \vec{\rho}_2)$  does not vary with  $z$ . For a path of length  $\ell_p$ , Eq. (11) then becomes

$$D_{\delta\phi}(\vec{\rho}_1, \vec{\rho}_2) = r_e^2 \lambda^2 \ell_p \langle [\Delta N_e(\vec{\rho}_1) - \Delta N_e(\vec{\rho}_2)]^2 \rangle \quad (12)$$

The integral can always be reintroduced to accommodate slow variations along the propagation path. The structure function automatically enters the theory as discussed in Section II. It has been recognized for some time, however, that the structure function intrinsically suppresses the low-frequency content of the field it is performed on.

To illustrate this directly, consider the one-dimensional form of Eq. (12). It is readily shown that

$$\langle [A(x) - A(x + \Delta x)]^2 \rangle = \int [1 - \cos(\omega \Delta x)] \Phi_A(\omega) \frac{d\omega}{2\pi} \quad (13)$$

where  $\Phi_A(\omega)$  is the power spectrum of  $A(x)$ . Since the cosine term in Eq. (13) varies as  $\omega^2$  for small  $\omega$ ,  $\Phi_A(\omega) \propto \omega^{-p}$  converges independent of any explicit outer-scale cutoff as long as  $p < 3$ . This is exactly the behavior of the one-dimensional phase structure functions for which  $p = 2\nu$  (Rino, 1979b). It might also be noted that Eq. (13) is identical in form to an MTI (Moving Target Identification) filter that is used for radar clutter suppression.

A convenient SDF model that is both mathematically tractable and accommodates inner-scale and outer-scale cutoffs is

$$\Phi_{\Delta N_e}(q) = C_s q_o^{2\nu+1} \sqrt{1 + (q/q_o)^2}^{(\nu+\frac{1}{2})} K_{\nu+\frac{1}{2}}(2\epsilon \sqrt{1 + (q/q_o)^2}) 2e^{-(\nu+\frac{1}{2})} / \Gamma(\nu+\frac{1}{2}) \quad (14)$$



where  $\epsilon = q_0/q_1 \ll 1$  is the ratio of the inner- to outer-scale cutoffs. By using the small-argument approximation,

$$K_{\nu+\frac{1}{2}}(2x) \sim \frac{1}{2} \Gamma(\nu + \frac{1}{2}) |x|^{-|\nu + \frac{1}{2}|}, \quad (15)$$

it is readily shown that for  $q \ll q_1$  and  $\epsilon \ll 1$ ,

$$\Phi_{\Delta N_e}(q) = \frac{C_s}{[q_0^2 + q^2]^{\nu+\frac{1}{2}}} \quad (16)$$

The phase autocorrelation function corresponding to Eq. (14) is

$$R(y) = \sigma_\phi^2 \sqrt{\epsilon^2 + (q_0 y/2)^2}^{\nu-\frac{1}{2}} K_{\nu-\frac{1}{2}}(2\sqrt{\epsilon^2 + (q_0 y/2)^2})/N \quad (17)$$

where

$$\begin{aligned} N &= 2\epsilon^{\nu-\frac{1}{2}} K_{\nu-\frac{1}{2}}(2\epsilon) \\ &\sim \Gamma(\nu - \frac{1}{2}) \end{aligned} \quad (18)$$

The approximation in Eq. (18) is good to within a few percent for  $\nu < 0.5$  and  $\epsilon < 0.01$ . In the small  $\epsilon$  approximation,

$$\sigma_\phi^2 = r_e^2 \lambda^2 \ell_p C_s \frac{\Gamma(\nu-\frac{1}{2})}{4\pi\Gamma(\nu+\frac{1}{2})} q_0^{-2\nu+1} \quad (19)$$

It is notationally convenient to let

$$C_p = r_e^2 \lambda^2 \ell_p C_s \quad (20)$$

so that the phase SDF has the form  $\Phi_{\delta\phi}(q) \sim C_p q^{-(2\nu+1)}$ . As noted in Section II, the fact that  $\sigma_\phi^2$  depends critically on  $q_0$  is indicative of its nonstationary behavior.

The form of the structure function that corresponds to Eq. (17) is

$$\mathcal{L}_{\delta\phi}(y) = 2\sigma_{\phi}^2 \mathcal{L}(y) = C_p \frac{\Gamma(\nu - \frac{1}{2})}{2\pi\Gamma(\nu + \frac{1}{2})} \left( \frac{\mathcal{L}(y)}{q_0^2 - 1} \right) \quad (21)$$

where

$$\mathcal{L}(y) = 1 - 2\sqrt{\epsilon^2 + (q_0 y/2)^2}^{\nu - \frac{1}{2}} K_{\nu - \frac{1}{2}}(2\sqrt{\epsilon^2 + (q_0 y/2)^2}) / N \quad (22)$$

In Figure 1,  $\mathcal{L}(y)$  is plotted versus  $q_0 y$  for  $\nu = 1.2$  and the  $\epsilon$  values 0.01, 0.001, and 0.0001. It is readily seen that the impact of  $\epsilon$  is negligible even for comparatively shallow SDFs where its effect is most pronounced. For  $\nu = 1.5$ , the corresponding curves, which are shown in Figure 2, cannot be distinguished.

Figure 3 shows the effect of varying  $\nu$ . At first glance the variations are not dramatic. It must be kept in mind, however, that the significant portion of the curve lies to the left of  $yq_0 = (2\pi)^{-1} = 0.159$ , since this corresponds to  $y \leq \ell_0 = 2\pi/q_0$ . As  $\nu$  increases, the curves are displaced to the right of  $y = \ell_0$ , indicating that structure is being determined more by  $q_0$  and less by the power-law slope.

If one accepts the mathematical form of Eq. (22) as being rigorously applicable, the  $\mathcal{L}(y)$  curves admit a simple interpretation. Indeed, from Eq. (10),  $R_{\nu}(\ell_d) = e^{-1}$  when  $\sigma_{\phi}^2 \mathcal{L}(\ell_d) = 1$ . It follows that plots of  $\mathcal{L}(y)$  versus  $yq_0$  are also plots of  $1/\sigma_{\phi}^2$  versus  $\ell_d q_0$ , provided that  $\sigma_{\phi} > 1$ . Since  $\mathcal{L}(\ell_d)$  saturates at unity, it is obvious that no meaningful definition of  $\ell_d$  can be obtained for small  $\sigma_{\phi}$  values. The fact that the definition of  $\ell_d$  depends on  $q_0$ , however, creates problems of its own.

As long as  $\nu < 1.5$ , there is a simple and effective way to deal with the latter situation that has been used in turbulence studies for over 30 years. It is shown in Appendix B that for sufficiently small  $q_0$ ,

$$\mathcal{L}_{\delta\phi}(y) \sim C_{\delta\phi}^2 |y|^{2\nu - 1} \quad (23)$$

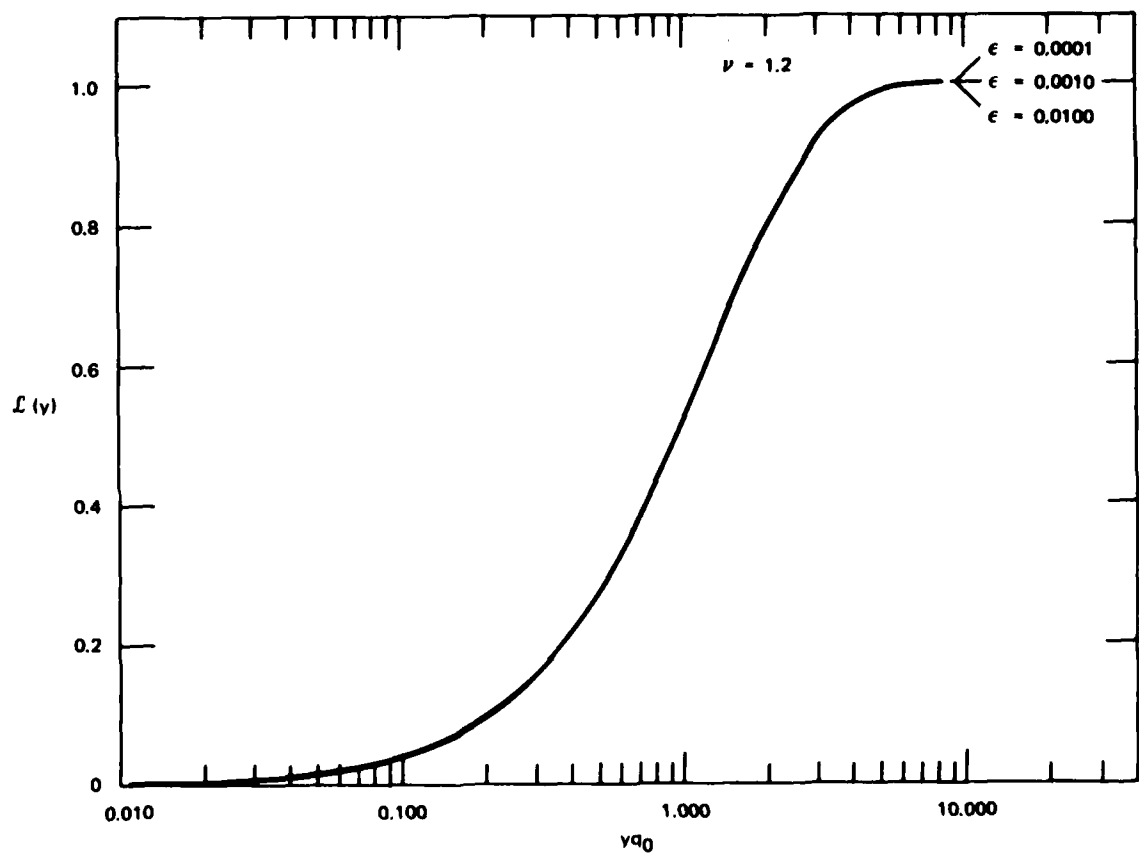


FIGURE 1 PLOT OF NORMALIZED PHASE STRUCTURE FUNCTION SHOWING EFFECT OF  $\epsilon$  FOR SHALLOWLY SLOPED PHASE SDF

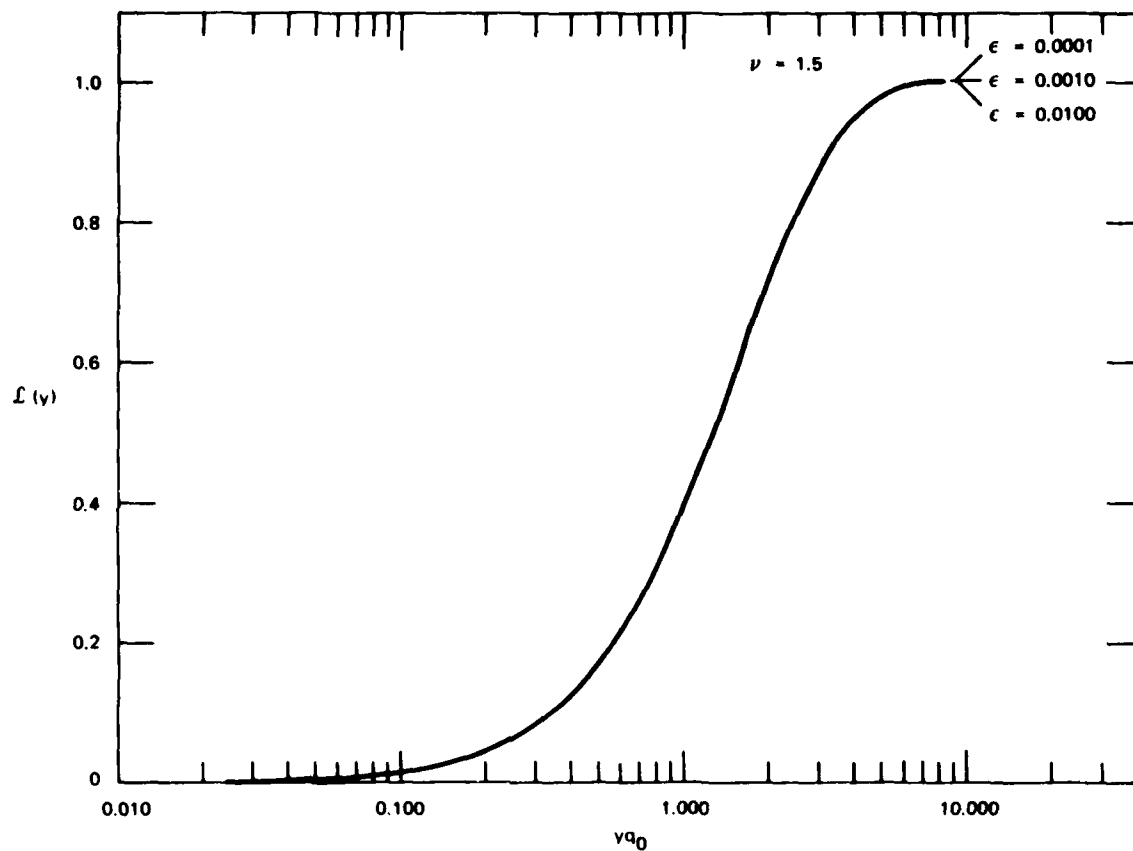


FIGURE 2 PLOT OF NORMALIZED PHASE STRUCTURE FUNCTION SHOWING EFFECT OF  $\epsilon$  FOR STEEPLY SLOPED PHASE SDF

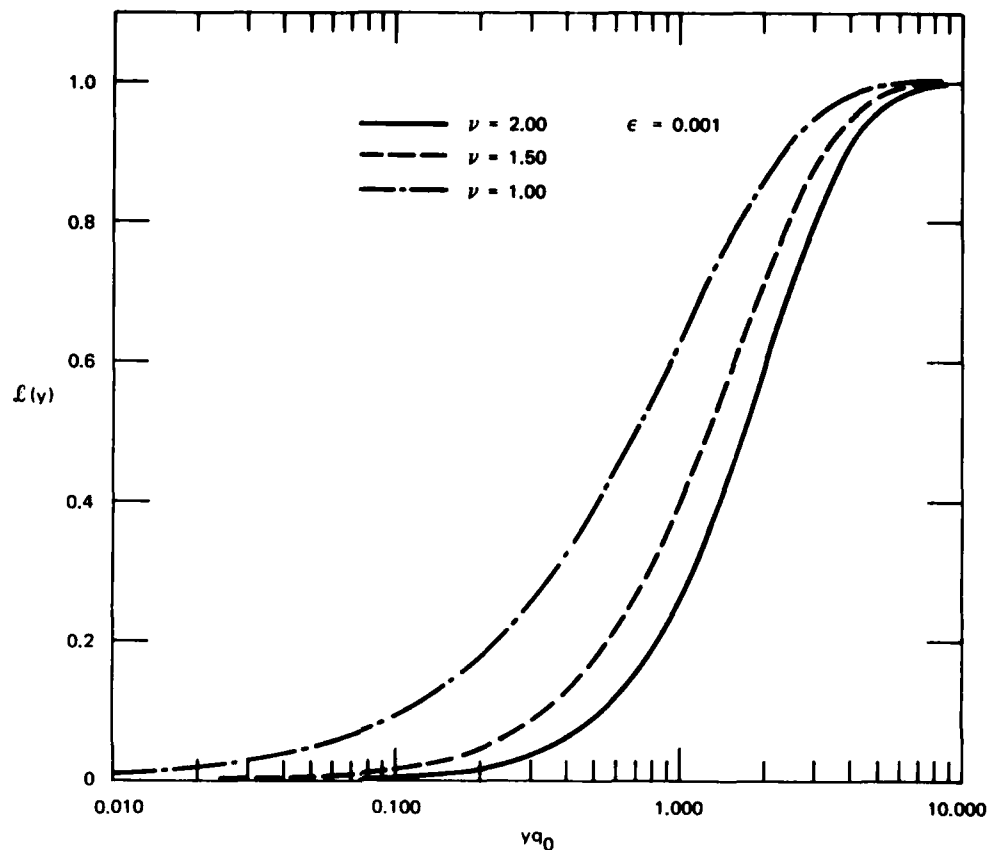


FIGURE 3 PLOT OF NORMALIZED STRUCTURE FUNCTION SHOWING DEPENDENCE ON SPECTRAL SLOPE

where

$$C_{\delta\phi}^2 = \frac{C_p}{2\pi} \frac{2(1.5 - \nu)}{\Gamma(\nu+0.5)(2\nu-1)^{2\nu-1}} \quad (24)$$

is the phase structure constant. To demonstrate the validity of this asymptotic approximation, the approximate form given by Eq. (23) is superimposed on the exact calculation of  $\mathcal{L}(y)$  in Figure 4.

The plot is presented on an expanded scale to emphasize the range of  $y$  values that contribute to the power-law continuum--viz,  $y < \ell$  [ $yq_0 < 0.159$ ]. For  $\nu \leq 1.2$ , the small  $q_0$  approximation works essentially over the entire  $y \leq \ell_0$  range. As the spectrum steepens ( $1.5 > \nu \geq 1.4$ ), the

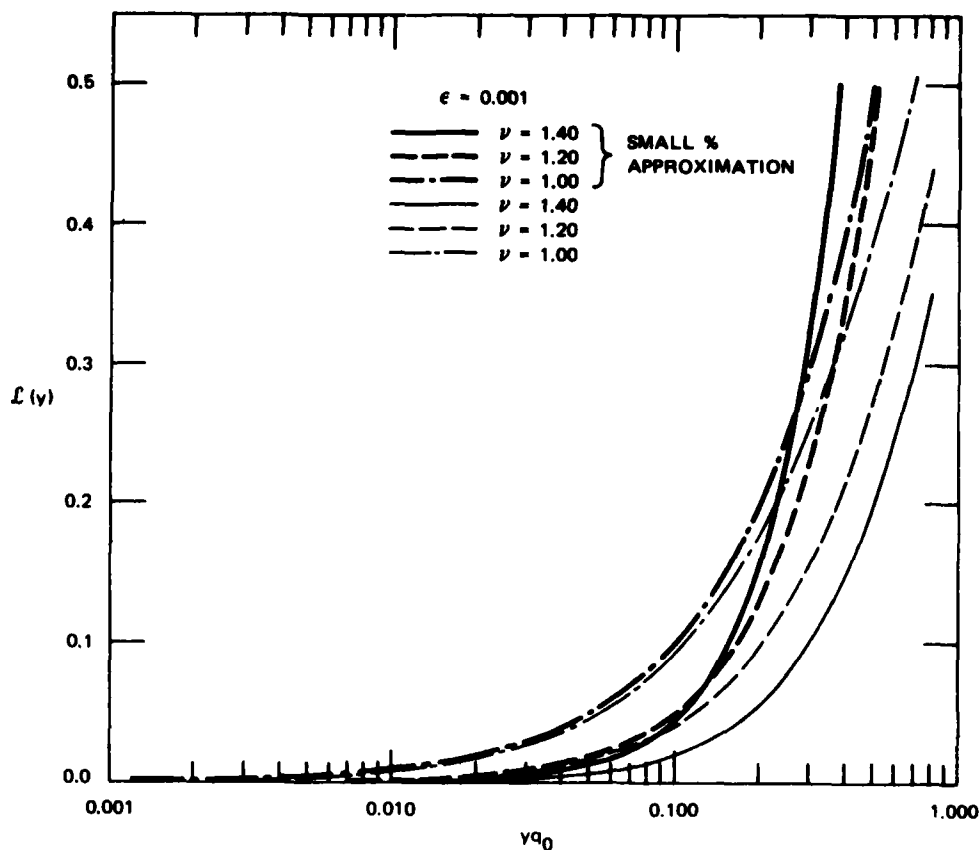


FIGURE 4 PLOT OF SMALL  $q_0$  APPROXIMATION TO PHASE STRUCTURE FUNCTION (valid for  $\nu < 1.5$ ) SUPERIMPOSED ON EXACT CURVES

$y \ll l_0$  condition becomes more stringent. Thus, as long as  $\nu \leq 1.4$ , the structure-constant approach is a viable one for the entire range of scale sizes that encompass the power-law continuum.

The ultimate test of any model, however, is how well it reproduces data. The Wideband satellite data have consistently shown  $p$  values less than 3. The range of  $\nu$  for Wideband is  $1.2 \leq \nu \leq 1.3$ . The Kolmogorov value is  $\nu = 4/3 = 1.333$ . Excellent results have been obtained in relating the intensity coherence time under strong-scatter conditions to estimates of  $C_{\delta\phi}^2$  from the phase data (Rino and Owen, 1979). In the analysis, Eq. (2) was effectively used to relate the intensity structure to  $C_{\delta\phi}^2$ . Equation (2) was, however, derived by calculating the strong-scatter limiting form of the fourth-order signal moment.

Attempts to measure the mutual coherence function directly have shown that Eq. (10) is strictly valid for a limited range of  $y$  values. For example, contrary to the predictions of Eq. (10), measured values of  $\langle v(t)v^*(t') \rangle$  invariably go negative. At the present time, attempts are being made to average several estimates together, but it appears that the departures from the idealized model are not simple random fluctuations that ultimately average out to the "correct" value.

What remains is to consider the situation for  $\nu \geq 1.5$ . As noted in Section I, the radio-wave propagation community has accepted the  $\nu = 1.5$  value as a norm, whereas the Wideband satellite data have consistently shown smaller values. The only carefully analyzed data that have indicated steeply sloped SDFs have come from in-situ equatorial rocket probes and in-situ as well as propagation data from the STRESS barium exercises. The early equatorial rocket probes can be dismissed since they only penetrated bottomside spread F. The preliminary results from the recent successful Kwajalein rocket campaign show that bottomside spread-F is a mere ripple when compared with well developed topside structures.

A barium cloud is a highly localized structure whose evolution can be optically tracked. A detailed analysis of the STRESS barium cloud ESTER by MRC has shown, firstly, that structures larger than 1 km cannot be reliably included in the power-law continuum, and secondly, that the smaller-scale structures fall off more steeply than  $K^{-2}$ .

The only radio propagation data were obtained from UHF transmissions that were highly disturbed. ESL has used a "back propagation" technique to reconstruct the integrated phase SDF, and the preliminary results seem to be in agreement with the in-situ data in that the phase SDF falls off more steeply than  $f^{-3}$ . Under such conditions, however, one should expect significant departures from Rayleigh statistics. The small size of the largest structure may make tests of the statistics difficult. A straightforward test of the back-propagation procedure, however, is to measure the mutual coherence function directly and see how it conforms to model calculations based on  $f(y)$  for  $\nu \geq 1.5$ .

One would like to believe that the barium data accurately reproduce what is happening locally. Over much larger regions, however, the integration over many structured subregions may well act to produce a shallower integrated phase spectral slope. In that case, the effective  $\nu$  index for calculating propagation effects is less than 1.5 and the diffraction theory is greatly simplified.

Recent analysis of 30-GHz scintillation data over long atmospheric paths has shown phase spectral slopes significantly lower than the expected  $8/3$  value based on the Kolmogorov theory. A random patch model has been invoked to reconcile the discrepancy. The model is supported by high-resolution radar data showing that clear-air turbulence develops in distinct narrow regions.

However the issue is resolved, there is a significant discrepancy between structure models inferred from the Wideband satellite data and the structure models that are being extracted from the STRESS barium data. The recent Kwajalein rocket data will undoubtedly shed some light on the issue, but it must be resolved if a viable predictive propagation code is to be developed.



#### IV THE TAYLOR SERIES APPROXIMATION

Several authors have applied a Taylor series approximation to  $\mathcal{L}(y)$  to simplify analyses involving integral expressions containing various combinations of structure functions (e.g., Taylor and Infosino, 1976; Buckley, 1971). As discussed by Rino (1979b), however, these series converge very slowly, particularly in the small  $q_0$  limit. In a recent analysis of sound propagation in sea water, Dashen (1977) concluded that the Taylor series approximation cannot be used in power-law medium.

Dashen, however, was concerned with SDF corresponding to  $\nu < 1.5$ , and the Taylor series approximation improves as  $\nu$  increases. Indeed, this is expected because the derivatives involved are equivalent to moments in the spectral domain. The moments are increasingly large unless the SDF falls off very rapidly. An inner-scale cutoff keeps the derivatives finite, but the convergence of the series is still very slow if, indeed, proper convergence even occurs.

In any case, the formal Taylor series expansion of  $\mathcal{L}(y)$  is easily derived. If we use the notation

$$R_{\nu-\frac{1}{2}}(z) = 2z^{\nu-\frac{1}{2}} K_{\nu-\frac{1}{2}}(2z)/N \quad (25)$$

and

$$f(y) = \sqrt{\epsilon^2 + (yq_0/2)^2} \quad (26)$$

it is shown in Appendix A that

$$\frac{\partial \mathcal{L}(y)}{\partial y} = R_{\nu-3/2}(f(y)) q_0^2 y/2 \quad (27)$$

From Eq. (27) all higher-order derivatives can be generated. For example,

$$\frac{\partial^2 f(y)}{\partial y^2} = -R_{\nu-5/2}(f(y)) q_0^4 y^2/4 + R_{\nu-3/2}(f(y)) q_0^2/2 . \quad (28)$$

In the  $y = 0$  limit,  $f(y) = \epsilon$ , and only the even derivatives survive. The formal Taylor series can be written as

$$f(y) = \sum_{n=1}^{\infty} D_n (q_0 y)^{2n} \quad (29)$$

where

$$D_n = \frac{\partial^{2n} f(y)}{(2n)! \partial y^{2n}} \Big|_{y=0} . \quad (30)$$

The coefficients are derived in Appendix A. For our purposes we need consider only the first coefficient,

$$D_1 = \frac{1}{2} \epsilon^{\nu-3/2} K_{\nu-3/2}(2\epsilon)/N \quad (31)$$

$$\cong \begin{cases} \frac{\Gamma(3/2-\nu)}{4\Gamma(\nu-\frac{1}{2})} \epsilon^3 & \nu < 3/2 \\ \frac{\log(2\epsilon)}{2\Gamma(\nu-\frac{1}{2})} & \nu = 3/2 \end{cases} . \quad (32)$$

From Eq. (32) we see that for  $\nu < 1.5$ ,  $D_1$  is very sensitive to  $\epsilon$ . In fact, the higher-order derivatives are even more sensitive to  $\epsilon$  and the Taylor series approach is useless, as noted by Dashen (1977). It appears that the series is divergent except for very small  $y$  values. The dependence on  $\epsilon$  decreases as  $\nu$  increases. If  $\nu > 1.5$ ,  $D_1$  does not depend on  $\epsilon$ , but higher derivatives do, and convergence problems persist.

In Figure 5 the quadratic approximation is shown for  $\nu = 1.2, 1.5$ , and  $2.0$ . The approximation is acceptable for  $\nu = 1.5$ , provided that  $y < l_0$ . It improved as  $\nu$  exceeds  $1.5$ , but the series approximation cannot be used, as we noted previously. We emphasize that neither the asymptotic nor the quadratic approximation admits  $y$  values larger than  $l_0 = 2\pi/q_0$ .

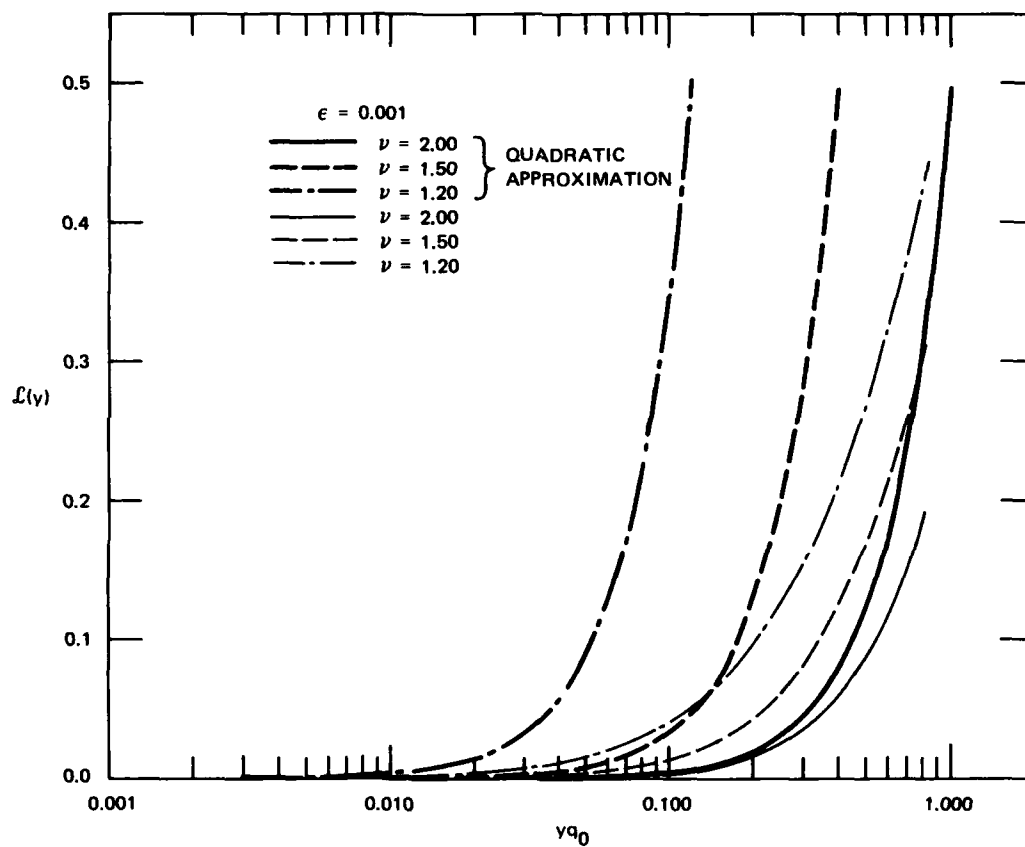


FIGURE 5 PLOT OF QUADRATIC APPROXIMATION TO PHASE STRUCTURE FUNCTION SUPERIMPOSED ON EXACT CURVES

## V SUMMARY AND DISCUSSION

In this report we have summarized some new results in propagation theory (Rino, 1979a,b,c; Rino and Owen, 1979), and have discussed their ramifications for predictive modeling. The theory was motivated by the Wideband satellite data which clearly showed the inhomogeneous structure of the integrated electron density. One observes slow trend-like variations in phase because of the dominance of large-scale structures in a power-law environment.

The large-scale structures potentially impact all signal moments. The impact can be nil or totally dominating, depending on the order of the moment and the power-law index. The first-order moment of the complex signal is exponentially dependent on the integrated phase; thus, it exhibits the same nonstationary behavior as the integrated phase.

The second-order complex signal moment (the mutual coherence function), which is used directly or indirectly for predicting essentially all strong-scatter propagation effects, is not sensitive to the large-scale structures if the effective spectral index  $\nu$  is less than 1.5, which is evidently the case for all naturally occurring irregularities. If  $\nu \geq 1.5$  as the STRESS data seem to indicate, the large-scale structures dominate the second-order moments. Predictive modeling then depends critically on the outer-scale parameter.

The Rayleigh hypothesis breaks down when  $\nu \geq 1.5$ . Insofar as system effects per se are concerned, departures from the gaussian model that is invariably used for analyzing or simulating disturbances are not too important. For predictive modeling of these parameters that characterize the signal structure, however, there is a significant impact.

Because of this fact we have suggested some independent checks of the back-propagation analysis of the STRESS scintillation data. Specifically, the departures from strict Rayleigh statistics, in particular  $S_4 > 1$ ,

that must accompany steeply sloped SDFs should be verified, if possible. The mutual coherence function itself should be carefully measured to verify that it conforms to model predictions.

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## Appendix A

### THE TAYLOR SERIES APPROXIMATION TO THE PHASE STRUCTURE FUNCTION

The normalized phase structure function can be written as

$$S(y) = 1 - \mathcal{R}_{\nu-\frac{1}{2}}(f(y)) \quad (\text{A-1})$$

where

$$\mathcal{R}_{\nu-\frac{1}{2}}(z) = 2z^{\nu-\frac{1}{2}} K_{\nu-\frac{1}{2}}(2z)/N \quad (\text{A-2})$$

$$N = 2\epsilon^{\nu-\frac{1}{2}} K_{\nu-\frac{1}{2}}(2\epsilon) \quad (\text{A-3})$$

and

$$f(y) = \sqrt{\epsilon^2 + (q_0 y/2)^2} \quad (\text{A-4})$$

It is clear from Eq. (A-4) that  $q_0$  is simply a scale factor. We shall derive a formal Taylor series representation for Eq. (A-1) with the aim of obtaining a simple approximation to  $S(y)$  that is valid for  $\epsilon \ll 1$ , and as large a  $yq_0$  range as possible.

To start with, consider the first derivative,

$$\frac{\partial S(y)}{\partial y} = - \frac{\partial \mathcal{R}_{\nu-\frac{1}{2}}(f(y))}{\partial y} \quad (\text{A-5})$$

The derivatives of products such as  $z^{\nu-\frac{1}{2}} K_{\nu-\frac{1}{2}}(2z)$  are known, and it is easily shown that

$$\frac{\partial \mathcal{R}_{\alpha} f(y)}{\partial \mathcal{R}} = -\mathcal{R}_{\alpha-1}(f(y)) q_0^2 y/2 \quad (\text{A-6})$$

Using Eq. (A-6) we have

$$\frac{\partial f(y)}{\partial y} = R_{v-3/2} (f(y)) q_o^2 y/2 \quad (A-7)$$

$$\frac{\partial^2 f(y)}{\partial y^2} = -R_{v-5/2} (f(y)) q_o^4 y^2/4 + R_{v-3/2} (f(y)) q_o^2/2 \quad (A-8)$$

and

$$\frac{\partial^3 f(y)}{\partial y^3} = R_{v-7/2} (f(y)) q_o^6 y^3/8 - 2R_{v-5/2} (f(y)) q_o^4 y/4 \quad (A-9)$$

The  $n^{\text{th}}$  derivative of  $f(y)$  has  $N_o = (n-1)/2+1$  terms if  $n$  is odd, and  $N_e = n/2+1$  terms if  $n$  is even. The first term always has the form

$$R_{v-1/2-n} (f(y)) q_o^{2n} y^n C_i^n \quad (A-10)$$

where

$$C_i^n = -1/2 C_i^{n-1} \quad (A-11)$$

We let  $C_i^n$  denote the coefficient of the  $i^{\text{th}}$  term in the  $n^{\text{th}}$  derivative. If  $n$  is odd, the terms  $i = 2, 3, \dots, N_o$  have the form

$$R_{(v-1/2)-n+(i-1)} q_o^{2(n-i+1)} y^{(n-2(i-1))} C_i^n \quad (A-12)$$

where

$$C_i^n = \left[ (n+3-2i) |C_{i-1}^{n-1}| + \frac{1}{2} |C_i^{n-1}| \right] (-1)^{n+2} \quad (A-13)$$

The same formula, Eq. (A-12), applies to the even derivatives, with the exception that the last coefficient,  $C_{n/2+1}^n$ , is equal to the previously computed last odd coefficient--i.e.,



$$C_{n/2+1}^n = C_{n/2}^{n-1} \quad (n \text{ even}) \quad . \quad (\text{A-14})$$

The formal Taylor series can be written as

$$f(y) = \sum_{n=1}^{\infty} D_n (y q_0)^{2n} \quad (\text{A-15})$$

where

$$D_n = \frac{\partial^{2n} f(y)}{(2n)! \partial y^{2n}} \Big|_{y=0} \quad . \quad (\text{A-16})$$

Only the  $N_e^{\text{th}}$  even term gives a finite contribution. Hence, from Eq. (A-12)

$$\begin{aligned} D_n &= \frac{1}{(2n)!} \mathcal{P}_{(\nu-1/2)-n} f(y) \Big|_{y=0} C_{n+1}^{2n} \\ &= \frac{1}{(2n)!} \epsilon^{\nu-1/2-n} K_{\nu-1/2-n}(2\epsilon)/N C_{n+1}^{2n} \quad . \end{aligned} \quad (\text{A-17})$$

Note that as long as  $\nu-1/2-n > 0$ ,  $D_n$  is nearly independent of  $\epsilon$  for small  $\epsilon$ . For large  $n$  values,  $D_n \propto \epsilon^{2\nu-1-2n}$ , which becomes arbitrarily large with increasing  $n$ . It follows that the range of applicability of the Taylor series approximation is very restrictive. Recent analysis by Dashen (1977) suggests that it can only be used for propagation environments with a sharp cutoff.

## Appendix B

### THE SMALL $q_0$ APPROXIMATION

Since  $\sigma_\phi \propto q_0^{-2\nu+1}$ , it follows that  $\sigma_\phi^2(1 - \mathcal{L}(y))$  converges to the indeterminate form  $\frac{0}{0}$  when  $yq_0 \ll 1$  and  $q_0$  is small. If  $\nu < 1.5$ , however, L'Hopital's rule can be applied to compute the limiting form of  $D(y) = \sigma_\phi^2(1 - \mathcal{L}(y))$ . We first let  $\epsilon \rightarrow 0$  to simplify  $\mathcal{L}(y)$  to

$$\mathcal{L}(y) \sim 1 - 2|q_0 y/2|^{\nu-1/2} K_{\nu-1/2}(q_0 y) / \Gamma(\nu-1/2) \quad (B-1)$$

which is the form used in Rino (1979b). The quantity of interest is

$$\lim_{q_0 \rightarrow 0} \frac{\mathcal{L}(y)}{q_0^{2\nu-1}} \quad (B-2)$$

Using the results of Appendix A to calculate the derivative of  $\mathcal{L}(y)$ , from L'Hopital's rule we have

$$\lim_{q_0 \rightarrow 0} \frac{\mathcal{L}(y)}{q_0^{2\nu-1}} = \lim_{q_0 \rightarrow 0} \frac{q_0 (q_0 y/2)^{\nu-3/2} K_{\nu-3/2}(q_0 y) y^2}{\Gamma(\nu-1/2)(2\nu-1)q_0^{2\nu-1}} \quad (B-3)$$

As long as  $\nu < 1.5$ , the small-argument approximation of  $K_{\nu-3/2}(q_0 y)$  shows that the  $q_0$  terms cancel and we have

$$\lim_{q_0 \rightarrow 0} \sigma_\phi^2(y) = \frac{C_p}{2\pi} \frac{2(1.5-\nu)}{\Gamma(\nu+0.5)(2\nu-1)2^{2\nu-1}} |y|^{2\nu-1} \quad (B-4)$$

This result has been used in studies of neutral turbulence for decades. The coefficient that multiplies  $|y|^{2\nu-1}$  is the phase structure constant.

In studies involving radio-wave interactions with turbulent neutral atmospheres, only the structure function enters the problem. Indeed, the structure constant is typically modeled directly. Only recently has

serious consideration been given to propagation effects in environments characterized by steeply sloped power-law SDFs.

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ATTN: S. Tashird  
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General Electric Co.  
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Ill. Sylvania, Inc.  
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Institute for Defense Analyses  
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ATTN: J. Aron  
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ATTN: W. Wolfhard

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Meteor Communications Consultants  
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Rockwell International Corp.  
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Tri-Com, Inc.  
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